## L 28001-66 ACC NR: AP6012496 served bands and of the temperature dependences of the intensities of the individual components with the published data leads to the conclusion that the observed effect is an optic analog of the Mossbauer effect in five different recombinations centers of silicon. Each band has a narrow line adjacent to a long-wave branch with a wellpronounced maximum. The narrow lines are due to phononless radiative transitions within the centers, and the long-wave components are due to radiative transitions with emission of acoustic phonons. The appearance of new bands during annealing is evidence of the complex nature of the centers. The authors thank P. S. Solov'yev for help with the preparation for the experiment. Orig. art. has: 1 figure and [02] SUB CODE: 20/ SUBM DATE: 040ct65/ ORIG REF: 004/ OTH REF: OOL/ ATD PRESS 4261 Card 2/2

L 40352-66 SWT(m)/EWF(t)/ETI IJF(c) GG/JD

ACC NR: AP6019223 SOURCE CODE: UR/0250/66/010/002/0080/0082

AUTHOR: Sevchenko, A. N.; Tkachev, V. D.

ORG: Belorussian State University im. V. I. Ienin (Belorusskiy gosudarstvennyy universitet)

TITLE: Photoconductivity spectra of p-type silicon irradiated with fast electrons

SOURCE: AN BSSR. Doklady, v. 10, no. 2, 1966, 80-82

TOPIC TAGS: photoconductivity, silicon, impurity center, irradiation effect, irradiation damage, Fermi level

ABSTRACT: The object of the work was to study the kinetics of formation and stability of radiation damage in p-type silicon irradiated with 1 MeV electrons at 25-30°C and integral doses of 10<sup>13</sup>-10<sup>18</sup> electrons/cm<sup>2</sup>. The change in the shape of the spectra of impurity photoconductivity was studied as a function of the irradiation dose. The effectiveness of the formation of radiation damage was found to depend on the impurity composition of the crystals. The shape of the spectrum of the photoconductivity signal depends on the position of the Fermi level in the forbidden zone. By raising or lowering the Fermi level, one can eliminate certain centers from the photoconductivity processes, which confirms the authors' earlier hypothesis that the structure of the spectra is related to volume defects, since the change in the position of the Fermi level reflects the conditions in the volume of the crystal. The observed change in the spec-

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L 27360-66 ENT(m)/EWP(t)/ETI IJP(c) JD  ACC NR: AP6011529 SOURCE CODE: UR/0250/66/010/007/01/19/0150	
AUTHORS: Sevchenko, A. N.; Tkachev, V. D.; Lugakov, P. F.;	
ORG: Belorussian State University im. V. I. Lenin (Belorusskiy	-
TITLE: Investigation of the influence of heat treatment on the photo- electric properties of silicon with radiation damages in its structure	
Double: AN BSSR. Doklady, v. 10, no. 3, 1966, 148-150	
TOPIC TAGS: silicon, single crystal, crystal structure, radiation damage, photoelectric property, heat effect, photoconductivity, fine	
ABSTRACT: The purpose of the investigation was to study the temperature stability of different radiation damages which are produced in single crystal silicon when irradiated with energy particles. The initial material was p-type silicon with resistivity 7 10 ohm-cm, containing	
3 8 x 10 <sup>17</sup> cm <sup>-3</sup> oxygen. The irradiation was with 1-Mev electrons from the stationary photoconductivity was plotted with apparatus described by	
Card 1/2	2

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L 27360-66
ACC NR. AP6011529  A. F. Plotnikov et al. (PTE, no. 3, 183, 1962). The results show that samples whose photoconductivity spectrum displayed no structure shortly samples whose photoconductivity spectrum displayed no structure after the cessation of the irradiation, acquired a pronounced structure after prolonged storage at liquid-nitrogen temperature. This is attribated to diffusion of the vacancy pairs resulting from the electron bomuted to diffusion of the vacancy pairs resulting from the electron bombardment. An increase in the temperature and longer storage following bardment. An increase in the point defects due to the bombardment to become the bombardment causes the point defects due to the bombardment to become the bombardment are interpreted and reconciled with the level annealed. The results are interpreted and reconciled with the level annealed. The results are interpreted and reconciled with the level is made difficult by the presence of different types of structure defects which can become transformed into each other during annealing. Orig.
SUB CODE: 20/ SUBM DATE: 14Jun65/ ORIG REF: 004/  Cord .2/2

SOURCE CODE: UR/0250/66/010/006/0374/0376 ACC NR: AP6021921 AUTHOR: Sevchenko, A. N.; Stel'makh, V. F.; Tkachev, V. D. ORG: Belorussian State University im. V. I. Lenin (Belorusskiy gosudarstvennyy universitet) TITLE: Photoelectric properties of gallium arsenide containing structure defects due to radiation SOURCE: AN BSSR. Doklady, v. 10, no. 6, 374-376 TOPIC TAGS: gallium arsenide, radiation effect, photoresistance, photoconductivity, resistivity, photoelectric property, fast neutron, neutron irradiation ABSTRACT: The energy spectrum of local levels in n- and p-type gallium arsenide single crystals irradiated with fast neutrons was investigated by studying the structure of photoconductivity spectra beyond the absorption edge. Spectral dependencies of photoconductivity were recorded at temperatures of 300 and 80K using samples with a resistivity up to  $10^{12}$  ohm. The specific resistivity of the irradiated samples was found to depend markedly on the density of neutron beams: at fluxes of  $10^{14}$  neutrons/cm<sup>2</sup> the resistivity increased slowly; at higher densities it increased rapidly, showing a tendency toward saturation at  $10^{17}$  neutrons/cm<sup>2</sup>. It was concluded that the irradiation of gallium arsenide produces a great number of stable combinations of point defects and residual chemical impurities. Orig. art. has: 2 figures. SUB CODE: 20/ SUBM DATE: 09Mar66/ ORIG REF: 002/ OTH REF: 002/ ATD PRESS: 603/

L 42097**-**66 EWT(m)/T/EWP(t)/ETI IJP(c) UR/0250/66/010/008/0550/0552 ACC NR: AP6029648 SOURCE CODE: Sevchenko, A. N.; Tkachev, V. D.; Urenev, V. I. AUTHOR: ORG: Belorussian State University im. V. I. Lenin (Belorusskiy gosudarstvennyy universitet) TITLE: Photoconductivity spectra of germanium single crystals irradiated with gamma-quanta SOURCE: AN BSSR. Doklady, v. 10, no. 8, 1966, 550-552 TOPIC TAGS: germanium single crystal, gamma irradiation, electron energy level, impurity level ABSTRACT: An investigation was made of the system of energy levels which appears in n-type and p-type germanium irradiated with gammaquanta from Co<sup>60</sup> at room temperature. Particular attention was given to a study of the stable centers which introduce deep energy levels into the forbidden zone. Photoconductivity spectra were taken in a range from 1 to 5 µ for temperatures from 300 to 80K before and after irradiation with integrated fluxes of  $10^{14}-5 \times 10^{17} \text{ kv/cm}^2$ . The specimens used were n- and p-type germanium single crystals with initial specific resistances of 48 ohm·cm and 6 ohm·cm, respectively. The concentration of residual impurities in the electrically active state for n-type Card 1/2

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L 42097**-**66 ACC NR: AP6029648 material was up to  $10^{12}$ — $10^{13}$  cm $^{-3}$ . Investigation of the electrical characteristics of specimens after irrativition thousand the presence of  $E_V$  + 0.01 eV,  $E_V$  + 0.008 eV, and  $E_V$  + 0.17 eV levels in p-type germanium and  $E_c$  - 0.20 ev level in n-type germanium. Irradiation of n-type crystals with doses up to 5 x  $10^{17}$  kv/cm<sup>2</sup> did not change the conductivity sign. At T = 80K the Fermi level in irradiated n-type specimens was located 0.16-0.22 ev from the bottom of the conductivity zone, while in p-type specimens it was found 0.20-0.26 ev from the top of the valence zone. The presence of deep centers in both irradiated and nonirradiated crystals indicates that these centers are not generated due to the irradiation but are only displayed as the result of The transition of electrons between the zones and these centers in irradiated crystals can lead to a significant change in the concentration of free carriers. Such a change in concentration is possible since after irradiation the equilibrated concentration of free carriers becomes very low as a result of their capture by the radiation damage; which introduces shallower energy levels. Therefore in irradiated specimens for which the ratio  $\Delta\sigma/\sigma$  is greater, it is nossible to detect deep energy levels which belong to residual imperfections of the crystal lattice. Orig. art. has: 1 figure. : [JA] -SUB CODE: 20/ SUBM DATE: 15Apr66/ ORIG REF: 002/ OTH REFT .002 ATD PRESS: 5064 Card 2/2 af

APPROVED FOR RELEASE: 07/16/2001 CIA-RDP86-00513R001755920016-5"

ACC NR. AP6033157

UR/0250/66/010/009/0641/0643 SOURCE CODE:

AUTHOR: Sevchenko, A. N. (Academician AN BSSR); Lomako, V. M.; Tkachev, V. D.

ORG: Belorussian State University im. V. I. Lenin (Belorusskiy gosudarstvennyy uni-

TITIE: Temperature and optical quenching of radiative recombination of gallium ar-

SOURCE: AN BSSR. Doklady, v. 10, no. 9, 1966, 641-643

TOPIC TAGS: gallium arsenide, luminescence quenching, radiative recombination, temperature dependence, absorption band, Raman spectrum

ABSTRACT: The purpose of the investigation was to determine the influence of temperature on the spectral distribution of the radiative recombination of electroluminescent diodes obtained from n-type GaAs by diffusion of beryllium, and the influence of constant external illumination in the intrinsic absorption band ( $\lambda \leq 0.83$  nm) on the intensity of the recombination band. The carrier density in the initial GaAs was  $8 \times 10^{17} - 6 \times 10^{18}$  cm<sup>-3</sup>. The optical resonators were made from the crystal by cleavage. The Raman spectra were investigated with apparatus based on the IKS-12 spectrometer. The radiation receiver was a germanium photodiode or a cooled FoS photoresistance. The constant illumination was with the aid of an incandescent lamp and a number of filters. The tests were made at temperatures 80 - 30K in a cryostat evacuated to 10-4 mm Hg. The radiative recombination without additional illumination

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EWI(m)/EWP(U)/ETI Jar(c) 4.-09**417-67** SOURCE CODE: UR/0020/66/169/003/0562/0564 ACC NRI AP6027951 AUTHOR: Sevenenko, A. H. (Academician All BSSR); Tkachev, V. D.; Lugakov, P. F. ORG: Belorussian State University im. V. I. Lenin (Belorusskiy gosudarstvennyy universitet) TITLE: Energy spectrum of radiation damage in silicon single crystals SOURCE: AN SSSR. Doklady, v. 169, no. 3, 1966, 562-564 TOPIC TAGS: silicon semiconductor, semiconductor band structure, crystal lattice defect, irradiation damage, impurity level ABSTRACT: The purpose of the investigation was to determine the energy levels that appear when the crystal is irradiated with different integral fluxes of 1-Mev electrons ( $10^{13} - 10^{18} \text{ el/cm}^2$ ), fast reactor neutrons ( $10^{12} - 10^{19} \text{ neut/cm}^2$ ), and  $\gamma$  quanta from  $\text{Co}^{60}$  ( $10^{15} - 10^{19} \text{ qu/cm}^2$ ). The initial n- and p-type crystals had a resistivity 0.03 -- 150 ohm-cm and a low concentration of impurities capable of producing deep levels in the forbidden band. The investigation consisted of measuring the temperature dependence of the conductivity and of the Hall coefficient, and the spectral distribution of the photoconductivity signal. The electrical measurements identified the principal donor and acceptor centers, while the photoelectric measurements identified the levels due to point defects and some of the chemical impurities. The results 537.312.5 Card 1/2

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cc NR: Ap6027951  how that the point defects give are conduction and valence band, this is interstitial atom pairs. A complete presented. Orig. art. has: 3 is presented. Ovig. art. has: 3 is presented.	ri oures.		near the e vacancy - ged silicon	
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ACC NR: AP6036960

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SOURCE CODE: UR/0181/66/008/011/3213/3217

AUTHOR: Yukhnevich, A. V.; Tkachev, V. D.; Bortnik, M. V.

ORG: Belorussian State University im. V. I. Lenin, Minsk (Belorusskiy gosudarstvennyy universitet)

TITLE: Annealing of bands of impurity recombination radiation in silicon irradiated with gamma quanta

SOURCE: Fizika tverdogo tela, v. 8, no. 11, 1966, 3213-3217

TOPIC TAGS: recombination radiation, radiative recombination, semiconductor carrier, gamma irradiation

ABSTRACT: The isochronous annealing of infrared radiation bands arising in silicon from the radiative recombination of excess carriers across the levels of radiation defects was studied. In the 25-600°C range, the successive appearance and disappearance of various bands was observed, indicating a complex character of the rearrangement of defects during annealing. The results obtained show an important role of oxygen in the formation of recombination centers in silicon upon irradiation with gamma quanta. On the other hand, this recombination radiation is a good indicator of low oxygen concentrations, and can be used to determine the latter. Thus, recombination radiation can be used as a means of studying the radiation defects of silicon and processes of their rearrangement during heat treatment. Nine different "radiating" radiation defects were observed, and the kinetics of their annealing showed the struc-

Card 1/2

#### ACC NR: AP6036960

ture of stable radiation defects to be complex. Oxygen atoms are an integral part of most of the radiation defects responsible for the observed bands of impurity recombination radiation. Phosphorus atoms participate in the formation of centers radiating D and E bands, and boron atoms take part in the formation of centers radiating F and Dands. The majority recombination centers (determining the lifetime of excess carriers) are annealed at 400-500°C. They are also linked to oxygen and are centers of nonradiative recombination. The intensity and energy distribution of the various bands of recombination radiation of silicon containing radiation defects and subjected to heat treatment permit an analysis of the content of chemical impurities in the initial single crystals. Both active (boron, phosphorus) and inactive impurities (oxygen) can thus be analyzed. Authors thank Z. M. Afanas yev and P. S. Solov yev for their systematic assistance in the course of the experiments. Orig. art. has: 1 figure and 1 table.

SUB CODE: 20/ SUBM DATE: 21Mar66/ ORIG REF: 006/ OTH REF: 008

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	New theorem on Usp. mat. nauk	k-twing, so analog to Wilson's the 20 no.;:74-175   -Ag 165.	acrem for primes. (MIRA 18:8)

TRACHEY, V.F. (Moskva); TRACHEY, Vl.F. (Voronezh)

Criterial for the absence of arbitrary and multiple limit cycles.
Mat. sbor. 52 no. 3:811-822 N '60.

(Differential equations)

(Differential equations)

## TRACHIV. V.F.

New sufficient conditions for stability, semistability and instability of the limit cycle of the  $\frac{1}{\sqrt{1}} = \frac{O(\sqrt{11})}{O(\sqrt{11})}$  equation. Dokl. AN SSSR 116 no.4:564-567 0 '57. (MIRA 11:3)

1. Voronezhskiy gosudarstvennyy universitet. Predstavleno akademikom P.S. Aleksandrovym.

(Differential equations)

16.3400

\$/039/60/052/003/003/007 C 111/ C 333

AUTHORS: Tkachev, V. F. (Moscow), Tkachev, Vl. F. (Voronezh)

TITLE: On Criteria for the Absence of Arbitrary and Multiple Limit Cycles

PERIODICAL: Matematicheskiy sbornik, 1960, Vol.52, No.3, pp.811-822 TEXT: The author considers the system

(1) 
$$\frac{dx}{dt} = P(x,y), \quad \frac{dy}{dt} = Q(x,y).$$

General theorem (Theorem 1): Let the system (1) be given in a simply connected domain G; let P and Q be continuous. WIf there are functions N(x,y), M(x,y) continuous in G, the partial derivatives of which are continuous in G and which possess the property that for the functions

h(x,y) = PM + QN and  $k(x,y) = \frac{\partial N}{\partial x} - \frac{\partial M}{\partial y}$  in G there holds one of

the following systems of signs

 $[\ge 0; = 0], [\le 0; = 0]; [= 0; \ge 0]; [= 0, \le 0]; [\ge 0; \le 0]$  or  $[\le 0; \ge 0]$ , then (1) possesses no limit cycles in G (the signs  $\le 0$  Card 1/9

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On Criteria for the Absence of Arbitrary and Multiple Limit Cycles and  $\geq$  0 mean that the function is = 0 at most on single curves and otherwise < 0 or > 0).

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Under the additional assumptions that P(x,y), Q(x,y) are continuous and continuously differentiable in G and that (whereever it is necessary) N(x,y), M(x,y) are twice continuously differentiable, the author collects in a scheme the most essential conditions (doubly framed) under which (1) possesses no limit cycles in G. Criteria based on the inverse signs ( $[\geq 0; \leq 0]$ ,  $[\leq 0; \geq 0]$ ) of the functions h(x,y) and k(x,y) must be used in the Green formula with regard to the sign.



Card 2/9

APPROVED FOR RELEASE: 07/16/2001 CIA-RDP86-00513R001755920016-5"

85226 S/039/60/052/003/003/007 0 111/ 0 333 On Criteria for the Absence of Arbitrary and Multiple Limit Cycles Scheme M(x,y)N(x,y)h(x,y)k(x,y)Remarks F(x,y) > 0FPM + FQN ≤0 General criterion **≡**0 37 < ≥ 0 1 M and N such that h > 0 everywhere in G  $F^2(P^2+Q^2)>0$ M = FPa N = FQM = F(P+Q)Ъ N = F(P+Q)M = F(P-Q)c N = F(Q-P)Card 3/9

APPROVED FOR RELEASE: 07/16/2001 CIA-RDP86-00513R001755920016-5"

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Į				
đ	$F^2(P^2+Q^2) > 0$	M = F(P+KQ) $N = F(-KP+Q)$	3x 3x 3x 3x ≤±0	K(x,y) ar- bitrary function
е	$F^2(P^2+Q^2) > 0$	M = F(P-KQ) $N = F(Q+KP)$	<u>∃ar(d+kb)</u> - <u>gr(b-kd)</u> <=0	ralize tho- se of Ben-
2	М	and N guch the	• —	dixon-Dulac
		and h such that	h = 0 everywhere in G	
a	FF'(PQ-PQ)≅0	M = -QF' $N = PF'$	$\frac{\partial x}{\partial x} + \frac{\partial y}{\partial y} \le \ge 0$	Criterion of Dulac
b	$F(PQ-PQ) \equiv 0$	F' = 1	$\frac{\partial P}{\partial x} + \frac{\partial y}{\partial Q} \le \ge 0$	Criterion of Bendixon
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S/039/60/052/003/003/007 On Criteria for the Absence of Arbitrary and Multiple Limit Cycles

	3	M and N su	ch that k	≡ 0 everywhere in G	
ε	i.	$\operatorname{FP} \frac{\partial K}{\partial x} + \operatorname{FQ} \frac{\partial K}{\partial y} \leq \geq 0$	$M = \frac{\partial K}{\partial x}$ $N = \frac{\partial K}{\partial y}$	$\frac{\partial^2 \mathbf{K}}{\partial \mathbf{x}  \partial \mathbf{y}} - \frac{\partial^2 \mathbf{K}}{\partial \mathbf{x}  \partial \mathbf{y}} \equiv 0$	Criterion of the type of H. Poincare
ъ	,	$P \frac{\partial K}{\partial x} + Q \frac{\partial K}{\partial y} \leq \geq 0$	F = 1	$\frac{9x9\lambda}{35^{K}} - \frac{9x9\lambda}{35^{K}} \equiv 0$	ralized Poin-
4		M and N suc	h that k	≥ O everywhere in G	care Criterion
a Cai		$F(P \frac{\partial K}{\partial x} + QN) \equiv \leq 0$ $N - \frac{\partial K}{\partial y} \text{ a mono-}$ $tone_{tone$		$\frac{\partial \mathbf{x}}{\partial \mathbf{w}} \cdot \frac{\partial \mathbf{x}}{\partial \mathbf{y}} = \frac{\partial \mathbf{x}}{\partial \mathbf{y}} = \frac{\partial \mathbf{x}}{\partial \mathbf{y}}$	

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On Criteria for the Absence of Arbitrary and Multiple Limit Cycles

5			Other cases	
а	≥ 0 2PQK ≤ 0 ≡ 0	M = FKQ N = FKP	$\frac{9x}{9^{Cb}} - \frac{9\lambda}{9^{Co}} \leq \frac{5}{9}$	C = FK
ь	P <sup>2</sup> -Q <sup>2</sup> 0	M = PF N = QF	$\frac{\partial FQ}{\partial x} + \frac{\partial FP}{\partial y} \stackrel{\leq}{\geq} \stackrel{=}{=} 0$	

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A cycle C is denoted as <u>multiple limit cycle</u> if for it

 $\int_{0}^{\infty} \left( \frac{\partial y}{\partial x} + \frac{\partial y}{\partial y} \right) dt$  vanishes, where l is the length of

C and the integration is carried out along the limit cycle in the direction of increasing t.

Theorem 2: Let P(x,y), Q(x,y) in (1) be continuous functions with

Card 6/9

s/039/60/052/003/003/007 C 111/ C 333

On Criteria for the Absence of Arbitrary and Multiple Limit Cycles

continuous partial derivatives in a simply connected domain G. If there are functions N(x,y)>0, M(x,y) continuous and continuously differentiable in G such that it is everywhere in G

$$P = \frac{\partial x}{\partial Mb} + \frac{\partial \lambda}{\partial M\delta} + \frac{\partial x}{\partial M} + \frac{\partial x}{\partial M} + \frac{\partial \lambda}{\partial M} + \frac{\partial \lambda}{\partial M} = 0 \quad (\ge 0)$$

and that h vanishes identically in no partial domain of G, then in G there are no multiple limit cycles of (!).

In theorem 3 the author gives four further criteria for the absence of multiple limit cycles. A generalized form of the first of these criteria is given in

theorem  $3^*$ : Let P(x,y), Q(x,y) be twice continuously differentiable in the simply connected domain G. Let twice continuously differentiable functions N(x,y) > 0 and M(x,y) exist such that

1.) the curves N(x,y) P(x,y) = 0 and N(x,y) Q(x,y) = 0 are representable as monotone functions y = f(x) and  $x = \varphi(y)$ ;

Card 7/9

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On Criteria for the Absence of Arbitrary and Multiple Limit Cycles

2.) the expressions  $A = \frac{\partial}{\partial x} \left( \frac{\partial NQ}{\partial y} + \frac{\partial}{\partial y} \frac{\partial}{\partial y} \right)$  and

$$B = -\frac{\partial \lambda}{\partial x} \left( \frac{\partial \lambda}{\partial Nb} + \frac{\lambda}{1} + \frac{\partial \lambda}{\partial N} \right)$$

are of constant and equal sign and both expressions do not simultaneously vanish identically;

3.) the signs of A and  $\frac{\partial NQ}{\partial y}$   $\frac{1}{NQ}$  +  $\frac{\partial M}{\partial y}$  (or of B and  $\frac{\partial NP}{\partial x}$   $\frac{1}{NP}$  +  $\frac{\partial M}{\partial x}$ ) are in a sufficiently small neighborhood of the curve  $x = \varphi(y)$  (y = f(x)) identical in the lower (upper) part of the plane under (above) the curve or, however,

$$\frac{\partial NQ}{\partial y}$$
  $\frac{1}{NQ}$  +  $\frac{\partial M}{\partial y}$  and  $\frac{\partial NP}{\partial x}$   $\frac{1}{NP}$  +  $\frac{\partial M}{\partial x}$ 

vanish identically, while in the other parts of the curves  $x = \psi(y)$  or y = f(x) these expressions have equal signs opposite to Card 8/9

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On Criteria for the Absence of Arbitrary and Multiple Limit Cycles

the sign of  $\Lambda$  or vanish identically.

Then (1) possesses no multiple limit cycles in G.

There are 3 figures, and 6 references: 3 Soviet, 2 French and 1 American.

SUBMITTED: March 6, 1959

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Card 9/9

20-4-11/51 On New Sufficient Conditions for the Stability, Semistability .. TKACHEU, V.F. On New Sufficient Conditions for the Stauffly, Semidave  $\frac{dy}{dx} = \frac{P(x,y)}{Q(x,y)}$  and Instability of the Limit Cycle of the Equation TKACHEV, V.F. AUTHOR: (O novykh dostatochnykh usloviyakh ustoychivosti, poluustoychivosti TITLE: (O novýkh dostatochnýkh uslovlýakh ustovomlyosti, politika  $\frac{dy}{dx} = \frac{p(x,y)}{Q(x,y)}$ ) i neustovchivosti predel'nogo tsikla uravneniya PERIODICAL: Doklad; Akademii Nauk SSSR, 1957, Vol. 166, Nr. 4, pp. 564-567 (USSR) Given the differential equation (1)  $\frac{dy}{dx} = f(x,y),$ where  $f(x,y) = \frac{P(x,y)}{Q(x,y)}$  and P(x,y) and Q(x,y) have partial ABSTRACT: derivatives of sufficiently high order. Let further L: x = \(\mathbb{X}(8)), y=ψ(s) (0≤s≤1) be a closed integral curve of (1). Then, according to Papush [Ref. 1], in a sufficiently small neighborhood of L (1) can be replaced by the equation  $\frac{dn}{ds} = F(s,n) ,$ card 1/3

On New Sufficient Conditions for the Stability, Semistability 20-4-11/51 and Instability of the Limit Cycle of the Equation  $\frac{dy}{dx} = \frac{P(x,y)}{Q(x,y)}$ 

where s is the arc length and n is the length of the normal. Theorem: The following conditions are sufficient for 1. stability (instability) of the cycle:

$$\int_{0}^{1} F_{n}^{i}(s,n) ds \Big|_{n=0} = 0,$$

$$\int_{0}^{1} F_{n}^{i} \exp \left[ \int_{0}^{s} F_{n}^{i} dt \right] ds \Big|_{n=0} = 0, \dots, \int_{0}^{1} F_{n}^{(k-1)} \left\{ \exp \left[ \int_{0}^{s} F_{n}^{i} dt \right] \right\} \frac{k-2}{ds} \Big|_{n=0}$$

$$\int_{0}^{1} F_{n}^{(k)} \left\{ \exp \left[ \int_{0}^{s} F_{n}^{i} dt \right] \right\} \frac{k-1}{ds} \Big|_{n=0} < 0 \quad (0>0) \quad k - odd,$$

2. semistability:

On New Sufficient Conditions for the Stability, Semistability and Instability of the Limit Cycle of the Equation  $\frac{dy}{dx} = \frac{P(x,y)}{Q(x,y)}$ 20-4-11/51

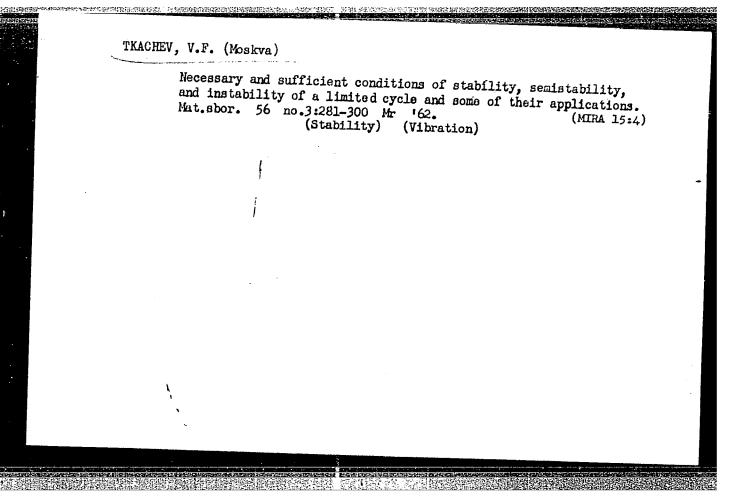
$$\int_{0}^{1} F_{n}^{i}(s,n) ds \Big|_{n=0} = 0, \qquad \int_{0}^{1} F_{n}^{(j)} \left\{ \exp \left[ \int_{0}^{s} F_{n}^{i} dt \right] \right\}^{j-1} ds \Big|_{n=0} = 0$$

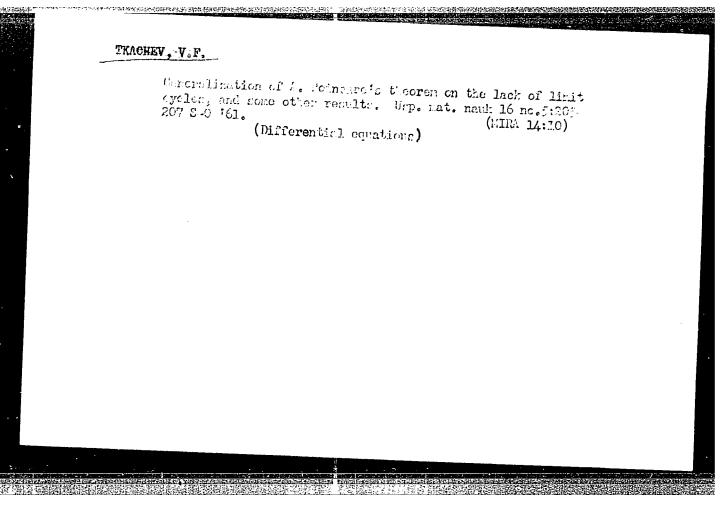
$$\int_{0}^{1} F_{n}^{(k)} \left\{ \exp \left[ \int_{0}^{s} F_{n}^{i} dt \right] \right\}^{k-1} ds \bigg|_{n=0} \neq 0 \qquad j=2,3,\ldots,k-1$$

ASSOCIATION: Voronezh State University (Voronezhskiy gosudarstvennyy universitet) PRESENTED BY: P. S. Aleksandrov, Academician, April 27, 1957

April 18, 1957 AVAILABLE: Library of Congress

Card 3/3





CHIGIRINETS, A.A.; TKACHEV, V.F.

Multiple machining of supports. Mashinostroitel' no. 4:30 Ap '61.

(Milling machines)

(MIRA 14:4)

TKACHEV, V.F. (Moskva); TKACHEV, VI.F. (Voronezh)

Criterial for the absence of arbitrary and multiple limit cycles.

Mat. sbor. 52 no. 3:811-822 N '60.

(Differential equations)

(MIRA 13:12)

16,3400

5/039/60/052/003/003/007

16.3400 C 111/ C 333 AUTHORS: Tkachev, V. F. (Moscow), Tkachev, Vl. F. (Voronezh)

TITLE: On Criteria for the Absence of Arbitrary and Multiple Limit Cycles

PERIODICAL: Matematicheskiy sbornik, 1960, Vol.52, No.3, pp.811-822 TEXT: The author considers the system

(1) 
$$\frac{dx}{dt} = P(x,y), \quad \frac{dy}{dt} = Q(x,y).$$

General theorem (Theorem 1): Let the system (1) be given in a simply connected domain G; let P and Q be continuous. WIf there are functions N(x,y), M(x,y) continuous in G, the partial derivatives of which are continuous in G and which possess the property that for the functions

h(x,y) = PM + QN and  $k(x,y) = \frac{\partial N}{\partial x} - \frac{\partial M}{\partial y}$  in G there holds one of

the following systems of signs

 $[\geq 0; \equiv 0], [\leq 0; \equiv 0]; [\equiv 0; \geq 0]; [\equiv 0, \leq 0]; [\geq 0; \leq 0]$ or  $[\leq 0; \geq 0]$ , then (1) possesses no limit cycles in G (the signs  $\leq 0$ 

s/039/60/052/003/003/007 c 111/ c 333

On Criteria for the Absence of Arbitrary and Multiple Limit Cycles and  $\geq$  0 mean that the function is = 0 at most on single curves and otherwise < 0 or > 0).

Under the additional assumptions that P(x,y), Q(x,y) are continuous and continuously differentiable in G and that (whereever it is necessary) N(x,y), M(x,y) are twice continuously differentiable, the author collects in a scheme the most essential conditions (doubly framed) under which (1) possesses no limit cycles in G. Criteria based on the inverse signs ( $[\ge 0; \le 0]$ ,  $[\le 0; \ge 0]$ ) of the functions h(x,y) and k(x,y) must be used in the Green formula with regard to the sign.



Card 2/9

CIA-RDP86-00513R001755920016-5

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 $\frac{\text{S/039/60/052/003/003/007}}{\text{C 111/ C 333}}$  On Criteria for the Absence of Arbitrary and Multiple Limit Cycles

#### Scheme

	h(x,y)	M(x,y) N(x,y) F(x,y)>0	К(x,y)	Remarks
	≥0 FPM + FQN ≤0 ≡0		$\begin{array}{ccc} 9x & 9\lambda < 5 & 0 \\ 9\mu & 9\overline{w} > \pm 0 \\ & \leq \pm 0 \end{array}$	General criterion
1	M	and N such th	nat h > 0 everywhere in G	
a	$F^2(P^2+Q^2) > 0$	M = FP N = FQ	3FQ - 3FP 3x 3FP≤±0	
ъ	$F^2(P^2+Q^2)^2>0$	M = F(P+Q) $N = F(P+Q)$		
С	$F^2(P-Q)^2 > 0$	M = F(P-Q) $N = F(Q-P)$	$\frac{\Im x}{\Im F(B-G)} - \frac{\Im A}{\Im F(B-G)} \leq \Xi O$	

Card 3/9

85226

S/039/60/052/003/003/007 C 111/ C 333 On Criteria for the Absence of Arbitrary and Multiple Limit Cycles

đ	$F^2(P^2+Q^2) > 0$	M = F(P+KQ) $N = F(-KP+Q)$	3x 3x 3y 3x	K(x,y) ar- bitrary function
е	$F^2(P^2+Q^2)>0$	M = F(P-KQ) $N = F(Q+KP)$	<u>Je(d+kb)</u> - <u>Je(b-kd)</u> ₹≥0	Criteria which gene- ralize tho- se of Ben- dixon-Dulac
2	M a	and N such that	h ≡ 0 everywhere in G	
a	FF'(PQ-PQ)≅0	M = -QF' N = PF'	$\frac{\Im x}{\Im F \cdot P} + \frac{\Im F \cdot Q}{\Im F \cdot Q} \le \ge 0$	Criterion of Dulac
ъ	$F(PQ-PQ) \equiv 0$	F' = 1	$\frac{\partial x}{\partial P} + \frac{\partial y}{\partial Q} \le \ge 0$	Criterion of Bendixon

Card 4/9

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S/039/60/052/003/003/007 C 111/ C 333

On Criteria for the Absence of Arbitrary and Multiple Limit Cycles

3	M and N suc	h that k	≡ O everywhere in G	
а	M and N such that $\frac{\partial K}{\partial x} + FQ \frac{\partial K}{\partial y} \le \ge 0$	$N = \frac{9\lambda}{9K}$ $M = \frac{9x}{9K}$	$\frac{3x  9\lambda}{3 \cdot 5} - \frac{3x  9\lambda}{5 \cdot K} \equiv 0$	Criterion of the type of H. Poincare
ъ			$\frac{9x9\lambda}{35^{\mathrm{K}}} - \frac{9x9\lambda}{35^{\mathrm{K}}} = 0$	Somewhat gene- ralized Poin- care Criterion
4	M and N su	ch that k	≥ O everywhere in G	
	$F(P \frac{\partial K}{\partial x} + QN) \equiv \leq 0$ $N - \frac{\partial K}{\partial y}  \text{a mono-}$ $\text{tone increasing}$	$\mathbf{M} = \frac{\partial}{\partial \mathbf{x}}$	$\frac{\frac{\partial \mathbf{x}}{\partial \theta}}{\frac{\partial \mathbf{x}}{\partial \mathbf{w}}} = \frac{\frac{\partial \mathbf{x}}{\partial \mathbf{x}}}{\frac{\partial \mathbf{x}}{\partial \mathbf{w}}} = \frac{\frac{\partial \mathbf{x}}{\partial \mathbf{x}}}{\frac{\partial \mathbf{x}}{\partial \mathbf{x}}} = \frac{\partial \mathbf{x}}{\partial \mathbf{x}} = \frac{\partial \mathbf{x}}{\partial \mathbf{x}}$	



85226

s/039/60/052/003/003/007 C 111/ C 333

On Criteria for the Absence of Arbitrary and Multiple Limit Cycles

5		-	Other cases	
а	2 0 2PQK ≤ 0 ≡ 0	M = FKQ N = FKP	$\frac{9x}{9cb} - \frac{9\lambda}{9c0} = 0$	C = FK
ъ	P <sup>2</sup> -Q <sup>2</sup> 0	M = PF N = QF	$\frac{\partial FQ}{\partial x} + \frac{\partial FP}{\partial y} \le 0$	

Ŋ

A cycle C is denoted as multiple limit cycle if for it

$$\int_{0}^{\ell} \left( \frac{\partial P}{\partial x} + \frac{\partial Q}{\partial y} \right) dt$$
 vanishes, where 1 is the length of

 $\boldsymbol{C}$  and the integration is carried out along the limit cycle in the direction of increasing  $\boldsymbol{t}_{\ast}$ 

Theorem 2: Let P(x,y), Q(x,y) in (1) be continuous functions with

Card 6/9

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s/039/60/052/003/003/007 c 111/ c 333

On Criteria for the Absence of Arbitrary and Multiple Limit Cycles

continuous partial derivatives in a simply connected domain G. If there are functions N(x,y)>0, M(x,y) continuous and continuously differentiable in G such that it is everywhere in G

$$P = \frac{\partial x}{\partial Mb} + \frac{\partial \lambda}{\partial M\delta} + \frac{\partial x}{\partial M} + \frac{\partial x}{\partial M} + \frac{\partial \lambda}{\partial M} + \frac{\partial \lambda}{\partial M} = 0 \quad (\ge 0)$$

and that h vanishes identically in no partial domain of G, then in G there are no multiple limit cycles of (1).

In theorem 3 the author gives four further criteria for the absence of multiple limit cycles. A generalized form of the first of these criteria is given in

theorem 3\*: Let P(x,y), Q(x,y) be twice continuously differentiable in the simply connected domain G. Let twice continuously differentiable functions N(x,y) > 0 and M(x,y) exist such that

1.) the curves N(x,y) P(x,y) = 0 and N(x,y) Q(x,y) = 0 are representable as monotone functions y = f(x) and  $x = \varphi(y)$ ;

Card 7/9

85226

s/039/60/052/003/003/007 C 111/ C 333

On Criteria for the Absence of Arbitrary and Multiple Limit Cycles

2.) the expressions  $A = \frac{\partial}{\partial x} \left( \frac{\partial NQ}{\partial y} + \frac{1}{NQ} + \frac{\partial M}{\partial y} \right)$ 

 $B = -\frac{\partial \lambda}{\partial x} \left( \frac{\partial x}{\partial Nb} + \frac{Nb}{1} + \frac{\partial x}{\partial W} \right)$ 

are of constant and equal sign and both expressions do not simultaneously vanish identically;

3.) the signs of A and  $\frac{\partial NQ}{\partial y}$   $\frac{1}{NQ} + \frac{\partial M}{\partial y}$  (or of B and  $\frac{\partial NP}{\partial x}$   $\frac{1}{NP} + \frac{\partial M}{\partial x}$ ) are in a sufficiently small neighborhood of the ox Mr (y = f(x)) identical in the lower (upper) part of the plane under (above) the curve or, however,

 $\frac{1}{NQ} + \frac{\partial M}{\partial y}$  and  $\frac{\partial NP}{\partial x} + \frac{1}{NP} + \frac{\partial M}{\partial x}$ 

vanish identically, while in the other parts of the curves  $x=\phi(y)$  or y=f(x) these expressions have equal signs opposite to

Card 8/9

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85226 s/039/60/052/003/003/007 c 111/ c 333

On Criteria for the Absence of Arbitrary and Multiple Limit Cycles

the sign of A or vanish identically.

Then (1) possesses no multiple limit cycles in G.

There are 3 figures, and 6 references: 3 Soviet, 2 French and 1 American.

SUBMITTED: March 6, 1959

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Card 9/9

s/042/61/016/005/005/005 0111/0444

A mineralisation of the theorem of H. Poincaré on the AUTHOR: absence of limit cycles and some other results TITLE:

PERIODICAL: Uspakhi matematicheskikh nauk, v. 16, no. 5, 1961,

A well-known theorem of Poincare for systems of second order is generalised as follows:

If in a certain domain G of the space  $(x_1, x_2, ..., x_n)$ there exists a continuous function  $N(x_1, x_2, ..., x_n)$  with continu-

ous partial derivatives such that

ous partial derivatives such that
$$h(x_1, x_2, ..., x_n) = \frac{\partial N}{\partial x_1} P_1 + \frac{\partial N}{\partial x_2} P_2 + ... + \frac{\partial N}{\partial x_n} P_n$$

has a constant sign and does not vanish in G, then the system

a constant sign and 
$$\frac{dx_{i}}{dt} P_{i}(x_{1}, x_{2}, ..., x_{n})$$
 (i = 1, 2,..., n) (2)

card 1/3

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s/042/61/016/005/005/005 C111/C444

A generalisation of the theorem...

does not possess any closed integral curves in G. Adjoining it is proved:

Adjoining It is provided in the system 
$$\frac{d^2x}{dt^2} = \int_1 (x, y) \frac{dx}{dt} + g_1(x, y) \frac{dy}{dt} + l_1(x, y),$$

$$\frac{d^2y}{dt^2} = \int_2 (x, y) \frac{dx}{dt} + g_2(x, y) \frac{dy}{dt} + l_2(x, y)$$

$$\frac{d^2y}{dt^2} = \int_2 (x, y) \frac{dx}{dt} + g_2(x, y) \frac{dy}{dt} + l_2(x, y)$$
(4)

where all functions  $f_i(x, y)$ ,  $g_i(x, y)$ ,  $l_i(x, y)$ , i = 1, 2, continuous and possess continuous partial derivatives, is defined in a simply connected domain G, and if there

a simply connected domain G, and The holds a simply connected domain G, and The holds 
$$h(x, y) = \frac{1}{1}(x, y) + \frac{1}{2}(x, y) > 0$$
 (<0)
$$h(x, y) = \frac{\partial}{\partial x} (g_1 + g_2) - \frac{\partial}{\partial y} (f_1 + f_2) > 0$$
 (<0)
$$h(x, y) = \frac{\partial}{\partial x} (g_1 + g_2) - \frac{\partial}{\partial y} (f_1 + f_2) > 0$$
 (<0)

then (4) does not possess any limit cycles in G.

h(x, y) = 
$$0x$$
 (81 by some solution of then (4) does not possess any limit cycles in G.

Theorem 3: If the system
$$\frac{d^3x}{dt^3} = m_1(x, y) \frac{d^2x}{dt^3} + n_1(x, y) \frac{d^2y}{dt^2} + l_1(x, y) \frac{dx}{dt} + g_1(x, y) \frac{dy}{dt} + l_1(x, y),$$

$$\frac{d^3x}{dt^3} = m_1(x, y) \frac{d^3x}{dt^3} + n_2(x, y) \frac{d^3y}{dt^3} + l_2(x, y) \frac{dx}{dt} + g_2(x, y) \frac{dy}{dt} + l_2(x, y),$$
(5)

Card 2/3  $\frac{d^3y}{dt^3} = m_2(x, y) \frac{d^3x}{dt^3} + n_2(x, y) \frac{d^3y}{dt^3} + l_2(x, y) \frac{dx}{dt} + g_2(x, y) \frac{dy}{dt} + l_2(x, y),$ 

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A generalisation of the theorem...

where all m, n, f, g, l are continuous, possessing continuous partial derivatives, is defined in a simply connected domain G, and if there

$$\frac{\partial (\mathbf{m}_1(\mathbf{x}, \mathbf{y}) + \mathbf{m}_2(\mathbf{x}, \mathbf{y}))}{\partial \mathbf{y}} + \frac{\partial (\mathbf{n}_1(\mathbf{x}, \mathbf{y}) + \mathbf{n}_2(\mathbf{x}, \mathbf{y}))}{\partial \mathbf{x}} \equiv 0$$

$$\frac{\Im(m_1(x, y) + m_2(x, y))}{\Im x} < 0 \quad (>0), \quad \frac{\Im(n_1(x, y) + n_2(x, y))}{\Im y} < 0 \quad (>0)$$

$$h(x, y) = 1_1(x, y) + 1_2(x, y) > 0 \quad (<0)$$

$$K(x, y) = \frac{\partial}{\partial x} (g_1 + g_2) - \frac{\partial}{\partial y} (f_1 + f_2) > 0 \quad (<0),$$

then (5) does not possess any limit cycles in G.

There is one Soviet-bloc reference and one non-Soviet-bloc reference.

SUBMITTED: February 3, 1960

Card 3/3

MARTYNOV, I.V.; KRUGLYAK, Yu.L.; MAKAROV, S.P.; TKACHEV, V.G.

Halo-A-nitrocarboxylic acids. Part 4: Derivatives of fluoro-chloro-A-nitroproprionic acids. Zhur.ob.khim. 33 no.10: 3388-3391 0 163. (MIRA 16:11)

APPROVED FOR RELEASE: 07/16/2001 CIA-RDP86-00513R001755920016-5"

EWT(m)/EWP(w)/EWA(d)/T/EWP(t)/EWP(z)/EWP(b) MJW/JD SOURCE CODE: UR/0369/65/001/006/0688/0693 L 14437-66 ACC NR: AP6002117 (N)

AUTHOR: Tkachev, V.I.; Kripyakevich, R.I.

ORG: Physicotechnical Institute, AN UkrSSR (Fiziko-tekhnicheskiy institut AN UkrSSR)

TITLE: On the role of hydrogen in the processes of steel failure in neutral corrosive

SOURCE: Fiziko-khimicheskaya mekhanika materialov, v. 1, no. 6, 1965, 688-693

TOPIC TAGS: hydrogen embrittlement, carbon steel, cathode polarization, mechanical fatigue, corrosion, sodium chloride

ABSTRACT: Low-cycle plastic fatigue (alternating deformation above the yield point) was studied on 08 KP steel (0.09% C, 0.37% Mn, 0.019% Si, traces of P and S) in order to determine low degrees of hydrogen absorption taking place in neutral electrolytes (3% NaCl solution). The specimens were subjected to bend tests beyond the elastic limits (plastic fatigue) at a frequency of 0.8 cps on an IMA IP-1 machine. A platinum spiral served as the anode during polarization. From the test results, "polarization curves," i.e., graphs of plastic fatigue (number of cycles up to failure) versus density of the cathodic polarization current were plotted. The curves obtained for the action of

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L 14415-66 EWP(z)/EWT(m)/EWP(b)/T/EWA(d)/EWP(w)/EWI(t) MJW/JD/WB ACC NR: AP6002126 (N) SOURCE CODE: UR/0369/65/001/006/0732/0733

AUTHOR: Tkachev, V. I.; Kripyakevich, R. I.; Kuslitskiy, A. B.; Kreymerman, G. I.

ORG: Physicomechanical Institute AN UkrSSR, L'vov (Fiziko-mekhanicheskiy institut AN UkrSSR)

TITIE: Effect of the purity of steel and corrosion medium on low-cycle fatigue

SOURCE: Fiziko-khimicheskaya mekhanika materialov, v. 1, no. 6, 1965, 732-733

TOPIC TAGS: steel, corrosion, durability, hydrogen embrittlement, sulfuric acid, sodium chloride, stress concentration

ABSTRACT: The effect of the content of nonmetallic inclusions on the low-cycle fatigue of annealed ShKh15 steel produced by various processes was studied in air and in corrosive media (3% NaCl solution; 0.1 N H2SO4 solution; 0.1 N H2SO4 solution with cathodic polarization at current density  $D_{\rm C} = 10~{\rm A/dm^2}$  corresponding to hydrogen absorption). Tests in air showed a marked divergence in the values of the durability of the purest and most contaminated steel. In the neutral medium, the durability drops by 15—25% while the effect of purity diminishes. In the acid medium, the durability drops even more (by 25—30%). Under hydrogen absorption conditions, the durability is at its minimum (about 60% of the value in air),

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ACC NR: AP6002126

And its dependence on the purity is slight; this is because the formation of brittle cracks tauses a decrease in durability. As the corrosiveness of the medium increases, the influence of steel purity of low-cycle fatigue levels off, probably because additional stress concentrators which are more effective than the nommetallic inclusions are formed. During hydrogen absorption, the inclusions act as sources of cracks. Orig. art. has: 2 figures.

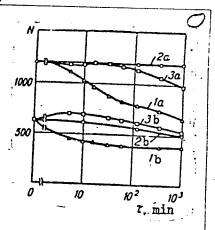
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Tkachev, V. I.; Aripyana ccp Livov (Fiziko-meknamien	
ACC NR: AP6020916  AUTHORS: Tkachev, V. I.; Kripyakevich, R. I.; Kuslitskiy, A. B.  ORG: Physico-Mechanical Institute, AN UkrSSR, L'vov (Fiziko-mekhanicheskiy)  ORG: Physico-Mechanical Institute, AN UkrSSR, Lovov (Fiziko-mekhanicheskiy)  Authors: Tkachev, V. I.; Kripyakevich, R. I.; Kuslitskiy, A. B.	
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ORG: Physico-Mechanical Institute, AN Oktoby institut AN UkrSSR)  TITLE: Influence of preliminary hydrogenation and corrosion on the low-cycle fatigue of steel  SOURCE: Fiziko-khimicheskaya mekhanika materialov, V. 2, no. 2, 1966, 192-194  SOURCE: Fiziko-khimicheskaya mekhanika materialov, V. 2, no. 2, 1966, 192-194  SOURCE: Fiziko-khimicheskaya mekhanika materialov, V. 2, no. 2, 1966, 192-194  SOURCE: Fiziko-khimicheskaya mekhanika materialov, V. 2, no. 2, 1966, 192-194  SOURCE: Fiziko-khimicheskaya mekhanika materialov, V. 2, no. 2, 1966, 192-194  SOURCE: Fiziko-khimicheskaya mekhanika materialov, V. 2, no. 2, 1966, 192-194  SOURCE: Fiziko-khimicheskaya mekhanika materialov, V. 2, no. 2, 1966, 192-194  SOURCE: Fiziko-khimicheskaya mekhanika materialov, V. 2, no. 2, 1966, 192-194  SOURCE: Fiziko-khimicheskaya mekhanika materialov, V. 2, no. 2, 1966, 192-194  SOURCE: Fiziko-khimicheskaya mekhanika materialov, V. 2, no. 2, 1966, 192-194  SOURCE: Fiziko-khimicheskaya mekhanika materialov, V. 2, no. 2, 1966, 192-194  SOURCE: Fiziko-khimicheskaya mekhanika materialov, V. 2, no. 2, 1966, 192-194  SOURCE: Fiziko-khimicheskaya mekhanika materialov, V. 2, no. 2, 1966, 192-194  SOURCE: Fiziko-khimicheskaya mekhanika materialov, V. 2, no. 2, 1966, 192-194  SOURCE: Fiziko-khimicheskaya mekhanika materialov, V. 2, no. 2, 1966, 192-194  SOURCE: Fiziko-khimicheskaya mekhanika materialov, V. 2, no. 2, 1966, 192-194  SOURCE: Fiziko-khimicheskaya mekhanika materialov, V. 2, no. 2, 1966, 192-194  SOURCE: Fiziko-khimicheskaya mekhanika materialov, V. 2, no. 2, 1966, 192-194	1 1
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TITLE: Influence of prefine the fatigue of steel  fatigue of steel  SOURCE: Fiziko-khimicheskaya mekhanika materialov, v. 2, no. 2, 1966, 192-194  SOURCE: Fiziko-khimicheskaya mekhanika materialov, v. 2, no. 2, 1966, 192-194  CORROSION RATE, HYDROSENATION, LOW CARBON STEEL, OSkp low  TOPIC TAGS: steel, alloy steel, hydrogen embrittlement, metal aging 08kp and  TOPIC TAGS: steel, shkhl5 carbon steel  Source: Fiziko-khimicheskaya mekhanika materialov, v. 2, no. 2, 1966, 192-194  CORROSION RATE, HYDROSENATION, LOW CARBON STEEL  OSKP and Corrosion RATE  TOPIC TAGS: steel, alloy steel, hydrogen embrittlement, metal aging 08kp and of annealed low-carbon steel  Source: Fiziko-khimicheskaya mekhanika materialov, v. 2, no. 2, 1966, 192-194  CORROSION RATE  OSKP 108kp low  TOPIC TAGS: steel, alloy steel, hydrogen embrittlement, metal aging 08kp and of annealed low-carbon steel  Source: Fiziko-khimicheskaya mekhanika materialov, v. 2, no. 2, 1966, 192-194  CORROSION RATE  OSKP 108kp low  CORROSION RATE  OSKP 108kp low  TOPIC TAGS: steel, shkhl5 carbon steel	a \
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followed and at a culture fig. 1). It was round hears a different	nhoiit
ABSTRACT:  of high-carbon steel Shkill We want to the experimental properties of high-carbon by B. I. Tkachev and R. I. The experimental properties of high-carbon by B. I. Tkachev and Yu. I. Babey (Fiziko-khimicheskaya mekhanika materialov, 1965, No. 2). The hydrogenation and corrosion of 2.5 x khimicheskaya mekhanika materialov, 1966, No. 2). The hydrogenation and corrosion of 3 amp/dm2. The mekhanika materialov, 1966, No. 2). The hydrogenation of 3 amp/dm2. The mekhanika materialov, 1966, No. 2). It was found that the mekhanika materialov, 1966, No. 2) are fig. 1). It was found that the mekhanika materialov and graphically (see Fig. 1). It was found different specimens was carried out in 3% NaCl at a current density of 3 amp/dm2. The experimental properties of the hydrogenation and corrosion and hydrogenation bears a different metal results are presented graphically (see Fig. 1). It was found that the mekhanika materialov, 1966, No. 2) are found to corrosion and hydrogenation bears a different metal results are presented graphically (see Fig. 1). It was found that the mekhanika materialov, 1966, No. 2) are found to corrosion and hydrogenation bears a different metal results are presented graphically (see Fig. 1). It was found that the mekhanika materialov, 1966, No. 2) are found to corrosion and hydrogenation bears a different metal results are presented graphically (see Fig. 1) are found to corrosion and hydrogenation bears a different metal results are presented graphically (see Fig. 1) are found to corrosion and hydrogenation bears a different metal results are presented graphically (see Fig. 1) are found to corrosion and hydrogenation bears a different metal results are presented graphically (see Fig. 1) are found to corrosion and hydrogenation bears a different metal results are presented graphically (see Fig. 1) are found to corrosion and hydrogenation bears a different metal results are found to corrosion and hydrogenation bears a different metal results are found to corrosion and hydrogenation bears a	Hoom
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L 42319-66

ACC NR: AR6020916

Fig. 1. Influence of the period,  $\mathcal{T}$ , of preliminary corrosion and hydrogenation on the number of cycles N for complete destruction of steel specimens OSkp (a) and ShKhl5 (b) respectively. 1 - preliminary hydrogenation; 2 - same, but followed by two hours of aging at 100C; 3 - preliminary corrosion.



by hydrogenation may be reversed by hydrogen desorption. The rate and degree of strength recovery depend on the composition of the steel; carbon and alloying elements decrease the tendency towards recovery. It is suggested that plastic fatigue experiments constitute a more sonsitive method for determining hydrogen than the rupture experiments. Orig. art. has: 2 graphs.

SUB CODE: 11/ SUBM DATE: 19Jan66/ ORIG REF: 004

Card 2/2 fdh

37941-66 EWT(m)/EWP(w)/T/EWP(t)/ETI IJP(c) JDACC NR AP6023448 SOURCE CODE: UR/0369/66/002/003/0336/0339 AUTHOR: Kuslitskiy, A. B.; Kreymerman, G. I.; Kokotaylo, I. V.; Starovoytov, Yu. Karpenko, G. V.; Tkachev, V. I. ORG: Physicomechanical Institute, AN UkrSSR, L'vov (Fiziko-mekhanicheskiy institut TITLE: Effect of metallurgical factors on the low-cycle fatigue in various media SOURCE: Fiziko-khimicheskaya mekhanika materialov, v. 2, no. 3, 1966, 336-339 TOPIC TACS: steel, low alloy steel, nickel containing steel, vacuum-decassed steel, low cycle-fatigue, ateel fatigue atrength, steel fatigue life/12KhN3A steel ABSTRACT: Low-allow 12KhN3A structural steel, conventionally cast or vacuum degassed, was hot-rolled into 40 mm plates or 3 mm sheets, hardened and tempered to a tensile strength of 100 dan/mm $^2$ , and tested for fatigue strength in the air, in a 3% NaCl aqueous solution, and in the same solution with applied cathodic polarization, the latter to promote a hydrogen absorption. A constant-amplitude, symmetrical bending at a frequency of 0.8 cps was used in the tests. The test results showed that vacuum-degassed steel had a longer fatigue life in all the investigated media than the conventionally cast steel, especially in the tests in the NaCl solution with cathodic polarization. The embrittling effect of hydrogen and, correspondingly, the difference in the fatigue life increased with increasing amplitude. Longitudinal Card

	specimens had a longer fatigue life than that of transverse specimens. With increasing amplitude, the difference in the fatigue life of longitudinal and transverse specimens increased substantially in tests in the air, and less so in tests in NaCl solution, but noticeably decreased in the NaCl with cathodic polarization. Sheet specimens had a slightly higher fatigue life than that of plate specimens in the air and in NaCl solution, but lower in NaCl with cathodic polarization. Orig.													
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35309 \$/039/62/056/003/001/004 B125/B102

11.3400

AUTHOR:

Tkachev, V. F. (Moscow)

TITLE:

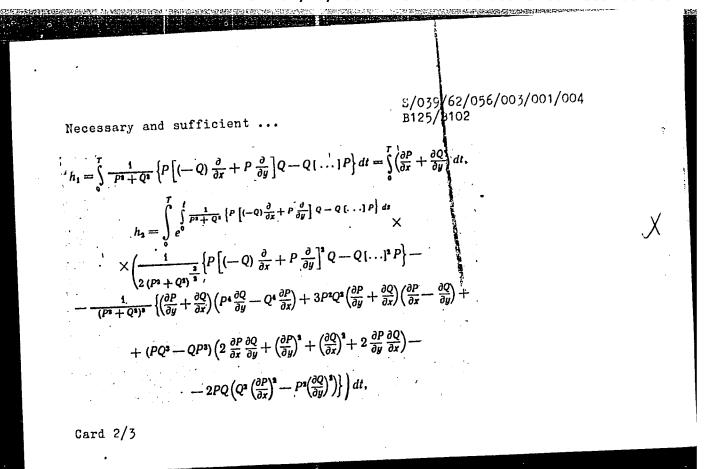
Necessary and sufficient conditions of stability, semistability, and instability of the limiting cycle and some of

their applications

PERIODICAL: Matematicheskiy sbornik, v. 56(98), no. 3, 1962, 281 - 300

TEXT: The author derives general criteria of stability and semi-stability of the limiting cycle L (x=x(t)=x(t+T), y=y(t)=y(t+T)) of the system dx/dt=P(x,y), dy/dt=Q(x,y). A sequence  $h_1$ ,  $h_2$ , is constructed in terms of which the criteria are formulated: If there is an odd number k such that  $h_1=0$ ,  $h_2=0$ , ...,  $h_{k-1}=0$ ,  $h_k<0$  (>0), then the limiting cycle L will be stable (unstable); if there is an even number k such that  $h_1=0$ ,  $h_2=0$ , ...,  $h_{k-1}=0$ ,  $h_k\neq 0$ , then the limiting cycle L will be semi-stable. The first two k read as follows:

Card 1/3



Necessary and sufficient ...

\$/039/62/056/003/001/004 B125/B102

These general criteria are specialized for so-called regular or monctonic limiting cycles. There are 15 references: 14 Soviet-bloc and 1 non-

SUBMITTED: January 11, 1960 (initially) September 1, 1961 (after revision)

Card 3/3

L 04923-67 EWT(d)/EWT(m)/EVP(w)/EWP(t)/ETI IJP(c) EM/JD/WB

ACC NR: AP6029687

SOURCE CODE: UR/0369/66/002/004/0457/0463

AUTHOR: Tkachev, V. I.; Kripyakevich, R. I.

ORG: Physics-Engineering Institute, AN UkrSSR, L'vov (Fiziko-mekhanicheskiy institut AN UkrSSR)

TITLE: Effect of characteristics of cyclic load on the low-cycle fatigue in media

SOURCE: Fiziko-khimicheskaya mekhanika materialov, v. 2, no. 4, 1966, 457-463

TOPIC TAGS: chromium steel, cyclic load, cyclic strength, corrosive strength, hydrogenation

ABSTRACT: Effects of amplitude, frequency, and asymmetry of cyclic deformation on the service life of steel in corrosive and hydrogenating environments was studied. High tempered 2.5 mm diam specimen of 12 KhN3A steel were exposed to 3% NaCl aqueous solutions and in the same solution under cathodic polarization to 10 a/dm² current densities, and tested at 1, 10, and 100 cycles/min and 0.5—8% amplitude of total deformation,  $\varepsilon$ . The amplitude of deformation was shown to be the dominating factor for service life. Stress characteristics

Card 1/2

L 01923-67 ACC NR: AP6029687

and alloy properties affected service life under experimental conditions much more than electrochemical conditions. At  $10-10^4$  cycles to failure,  $\epsilon N^m = C$ , N being the number of cycles and m and C constants. The effect of environment decreases with increasing amplitude of deformation and no essential effect of corrosivity is observed if the amplitude reaches a critical value. Under uniform amplitudes of deformation and at low-cycle tests in air, service life is hardly affected by the asymmetry of cycles. Service life in a hydrogenating medium increased at the transition from asymmetry to symmetry of the cycle. Effects of environment on service life decreased with increasing frequencies of cyclic stress, particularly in hydrogenating and, to a lesser degree, in corrosive environments. The value of the critical amplitude decreases with increasing frequency. Orig. art. has: 2 formulas, 2 tables, and 4 figures.

SUB CODE: 11/ SUBM DATE: 03Mar66/ ORIG REF: 005/ OTH REF: 006

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Card 2/2

SOURCE CODE: UR/0369/66/002/004/0464/0467 EM/JD EWT(d)/EWT(m)/EWP(w)/EWP(t)/ETI L 04941-61 ACC NRI

AUTHOR: Tkachev, V. I.; Kripyakevich, R. I.; Kuslitskiy, A. B.; Kreymerman, G. I.

ORG: Physics-Engineering Institute, AN UkrSSR, L'vov (Fiziko-mekhanicheskiy institut

AN UKrSSR)

TITLE: Effect of stress concentration on low-cycle fatigue in media

SOURCE: Fiziko-khimicheskaya mekhanika materialov, v. 2, no. 4, 1966, 464-467

TOPIC TAGS: stress concentration, material deformation, corrosive strength, hydrogenation, cyclic strength, fatigue strength

ABSTRACT: The effect of the amplitude of total deformation,  $\epsilon$ , and of stress frequency,  $\nu$ , on the low-cycle fatigue of specimens was studied with concentrators of stress, represented by 1 mm holes in the flat samples. The latter were tested in air and in corrosive and in hydrogenating environments. Concentration of stress resulted in a marked decrease of service life under low-cycle fatigue as compared with conditions of uniform stress distribution. The value N(ε), N being the number of cycles, showed the same basic dependence upon conditions as under uniform stress. The value of critical deformation decreased at a concentration of

Card 1/2

CIA-RDP86-00513R001755920016-5" **APPROVED FOR RELEASE: 07/16/2001** 

uniform	stress. The dependence of the effective coefficient of stress concentration on deformation amplitude and stress frequency was determined by the ratio of the environment factors for uniform stress and concentrated stress, respectively. Orig. art. has: 3 figures.									
SUB COD	E: 11/	SUBM DATE:	03Mar66/	ORIG REF:	001/	OTH REF: 011				
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#### TKACHUK, V.K.

Respiratory fluctuations of the ballistocardiogram in hypertension treated in a biotron. Vrach. delo no.1:25-28 Ja'64 (MIRA 17:3)

1. Kafedra terapii i kafedra nervnykh bolezney Kiyevskogo instituta usovershenstvovaniya vrachey. Nauchnyye rukovoditeli chlen- korrespondent AMN SSSR, prof. D.F. Chebotarev i zasluzhennyy deyatel! nauki prof. D.I.Panchenko.

TKACHEV, V.K., mashinist teplovoza

Diesel locomotive engineer V.K. Tkachev shares his experience.
Elek. i tepl. tiaga no.6:41-42 Je '58. (MIBA 11:6)

1.Depo Orsk, Orenburgskaya doroga.
(Diesel lecomotives)

APPROVED FOR RELEASE: 07/16/2001 CIA-RDP86-00513R001755920016-5"

TKACHEV, V.K.

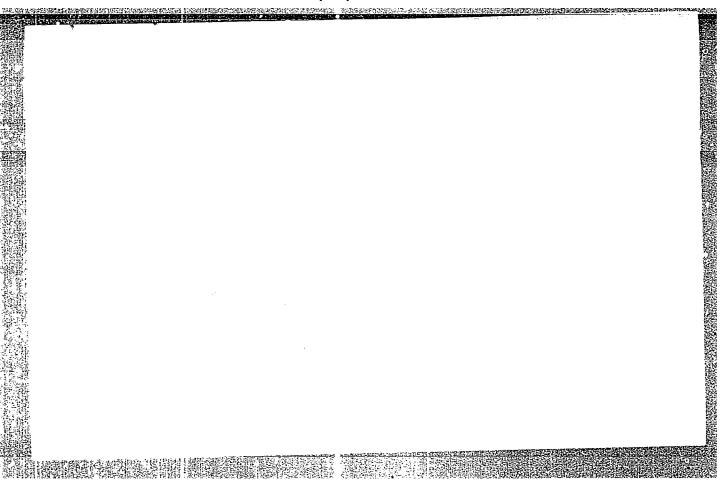
Maintenance of TE3 diesel locomotives during winter. Elek. i tepl. tiaga 2 no.1:18-19 Ja '58. (MIRA 11:3)

1. Starshiy mashinist teplovoza TE), depo Orsk, Orenburgskoy dorogi.
(Diesel locomotives--Cold weather operation)

APPROVED FOR RELEASE: 07/16/2001 CIA-RDP86-00513R001755920016-5"

Upper Paleozoic tuff lavas and ignimorites of the Kurama Range.
Trudy Lab. vulk. no.20:199-205 '61. (MIRA 14:11)

1. Glavgeologiya Uzbekskoy SSR. (Kurama Range--Vocanic ash, tuff, etc.)



TKACHEV, V. N., Cand Tech Sci -- (diss) "Corrosion Damage to the Metal of Locomotive Furnaces." Khar'kov, 1957. 12 pp (Min of Railways USSR, Khar'kov Inst of Engineers of Railway Transportation im S. M. Kirov), 110 copies (KL, 49-57, 113)

- 41 -

TEACHEV, V.N., kand. tekhn. nauk, dots., rod.; PIECHUE, A.F., rod.

[Induction hard facing with wear-resistant alleys] Induktisionmaia naplayka iznosostoikikh splavov; abornik statel. dostov-na-Donu, OhTl 1963. 112 p. (KIRA 1749)

1. Rostovskiy-na-Donu nauchno-issledovatel skiy institut tekhnologii mashinostroyeniya (for Trachev).

KISLIK, V.A., doktor tekhn. nauk, prof.; TKACHEV, V.N., inzh.

Local corrosion of metal in steam locomotive boilers. Trudy RIIZHT no.23:170-216 58.

(Locomotive boilers—Corrosion)

APPROVED FOR RELEASE: 07/16/2001 CIA-RDP86-00513R001755920016-5"

TKACHEV, V.N., kand.tekhn.nauk; SHVEDIAOV, N.M., inzh.

Self-grinding cutting parts of milling cutters. Trakt. i sel'khozmash.
(MIRA 15:1)

1. Rostovskiy nauchno-issledovatel'skiy institut tekhnologii
mashinostroyeniya.

(Peat machinery)

KISLIK, V.A., doktor tekhn.nauk, prof.: TKACHEV, V.N., kand.tekhn.nauk

"Investigating the wear of metals" ty M.M.Khrushchov, M.A.Babichev.
Reviewed by V.A.Kislik, V.N.Tkachev. Vest.mash. 41 no.8:87-88
Ag '61. (Mechanical wear)

(Khrushchov, M.M.) (Babichev, M.A.)

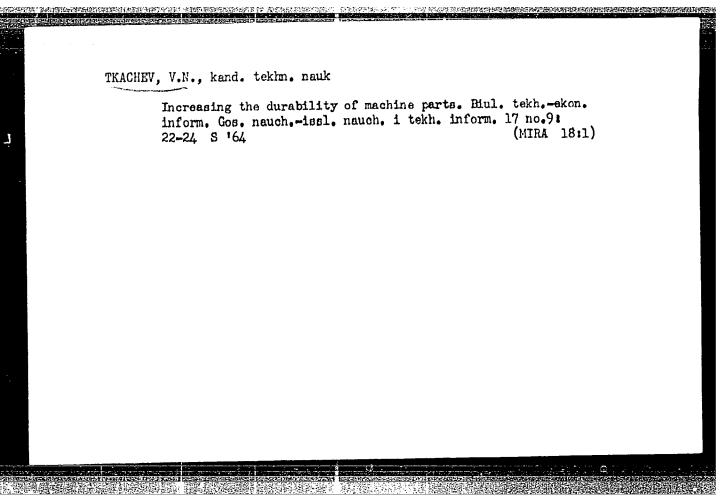
APPROVED FOR RELEASE: 07/16/2001 CIA-RDP86-00513R001755920016-5"

TKACHEV, V.N., kand.tekhn.nauk; SMOVT, M.S., inzh.

Built-up welding of cultivator sweeps using sormite and highfrequency currents. Trakt.i sel'khozmash. 32 no.4:42-45 Ap 162. (MIRA 15:4)

1. Rostovskiy-na-Donu nauchno-issledovatel'skiy institut tekhnologii mashinostroyeniya.

(Cultivators--Maintenance and repair)



L 11108-66 (/) EWT(m)/EWP(e)/EWP(v)/T/EWP(t)/EWP(z)/EWP(b)/EWP(b)/EWA(c) ID/HM/H ACC NR. AP6002531 . SOURCE CODE: UR/0286/65/000/023/0036/0036	I
INVENTOR: Petrov, S. A.; Kaufman, M. S.; Kialyuk, P. I.; Zhuravlev, V. L.; Krichevskiy, Z. A.; Aldyrev, D. A.; Kazintsev, N. V.; Tkachev, V. N.  ORG: none	
TITLE: Method of strengthening thin-sheet parts. Class 21, No. 176646. [an-nounced by the All-Union Scientific Research and Design Technological Institute of Coal Machine Building (Vsesoyuznyy nauchno-issledovatelskiy i proyektno-tekhno-logicheskiy institut ugol'nogo mashinostroyeniya); Rostov Scientific Research Technological Machine Building Institute (Rostovskiy nauchno-issledovatel'skiy institut tekhnologii mashinostroyeniya)	
SOURCE: Byulleten' izobreteniy i tovarnykh znakov, no. 23, 1965, 36  TOPIC TAGS: thin sheet part, part strengthening, part surfacing, thin sheet is surfacing, wear resistant powder	
ABSTRACT: This Author Certificate introduces a method of strengthening thin—  sheet parts by surfacing with wear-resistant powder deposited with high-frequency current. To maintain a constant gap between the inductor and the surfaced part, ensure a small depth of penetration in the base metal, and to avoid burning through, the inductor is located below the surfaced part.	
SUB CODE: 11/ SUBM DATE: 24Nov62/ ATD PRESS: 4/76 Card 1/1 H(x) UDC: 621.791.927-415	-
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L Oh5h9-67 EWT(d)/EWT(m)/EWF(t)/EVF(t)/ETI/EWF(h)/EWF(1) IJF(c) JU ACC NRi AP6023439 (A) SOURCE CODE: UR/0135/66/000/007/0024/0026

AUTHOR: Tkachev, V. N. (Candidate of technical sciences); Aldyrev, D. A. (Engineer)

ORG: NIITM, Rostov-on-the-Don (NIITM)

TITLE: Induction surfacing of thin-walled metal objects with wear-resistant alloys

SOURCE: Svarochnoye proizvodstvo, no. 7, 1966, 24-26

TOPIC TAGS: induction hardening, wear resistant alloy, conveying equipment

ABSTRACT: The results of testing induction-surfaced "trough" of scraper conveyers are presented. Due to thermal effect on the surface, induction surfacing causes considerable warpage in the sheet metal. By clamping the work as shown in figure 1, the maximum warpage is reduced 25 times compared with an unclamped sheet. Two methods of placing inductors were used: from the side of the deposited layer, and from the other side. The second method is more efficient in that the inductor is closer to the workpiece. With a metal thickness of 3 mm and a frequency of 70 kilocycle, the current penetration is 2.6 mm. About 86.5% of the induced energy is turned into heat in this area. The other 13.5% of the energy input is released in the 0.4 mm of the sheet. Hence, it follows that the heat input is evenly spread throughout the entire thickness. In order to deposit 4 areas 140 × 30 mm, a special inductor was designed. It has an F100 ferritic magnet for increasing its efficiency. The F100 has a permeability coefficient of 100

UDC: 621.791.927.7:621.3.023:669.018.25

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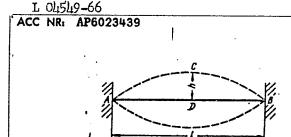


Fig. 1. Scheme of deformation of the coated zone.

and a maximum working temperature of 350°C. The depositing inductor is supplied from the LZ-107 high-frequency source (rating 100 kw, frequency 70 kilocycle, deposition area 140 × 25 mm, layer thickness 0.75 ± 0.25 mm). Deposition regime: time--25-30 sec, power consumption--1.1-1.2 (mw/hr), anode voltage--11 kv, contour voltage--4.5-6 kv, anode current--16-13 ka, grid current--2.8-3a. Under the above conditions, the sheet metal did not warp. However, due to internal stresses, some warpage took place during cooling. Therefore, the sheet must be water cooled before unclamping. This process is called "thermal fixing" and according to the micrographic tests it produced neither micro- nor macro-cracks. The Rockwell hardness of the surface was 48-52. The coated troughs are 1.8 times more wear-resistant compared with the uncoated troughs. Orig. art. has: 5 figures.

SUB CODE: 11.13/ SUBM DATE: none

Card 2/2 JS

TKACHEV, V.N.; RADCHENKO, A.T.; FISHTEYN, B.M.

Characteristics of the white layer formation on cog wheels.
Metallowed. i term.obr.met. no.1:47-49 Ja '65.

1. Rostowskiy nauchno-issledovatel'skiy institut tekhnologii
mashinostroyeniya.

(MIRA 18:3)
mashinostroyeniya.

TKACHEV, V.N., kand. tekhn. nauk; FISHTEYN, B.M., inzh.

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Some factors determining the structure and wear resistance of hard facing deposited as sormite. Avtom. svar. 17 no.11:57-64 N \*64 (MIRA 18:1)

1. Rostovskiy-na-Donu nauchno-issledovatel'skiy institut tekhno-logii mashinostroyeniya.

APPROVED FOR RELEASE: 07/16/2001 CIA-RDP86-00513R001755920016-5"

(MIRA 16:6)

# TKACHEV, V.N. Methods of studying the abrasion of metals. Zav. lab. 29 no.6:758-760 163. (MIRA 16:6)

(Metals—Testing) (Abrasion)

APPROVED FOR RELEASE: 07/16/2001 CIA-RDP86-00513R001755920016-5"

TKACHEV, V.N., kand.tekhn.nauk; KAZINTSEV, N.V., inzh.

High-frequency hard facing with sormite of self-dressing plowshares. Svar.proizv. no.1814.—16 Ja \*63. (MIRA 16:2)

1. Nauchno-issledovatel'skiy institut tekhnologii mashinostroyeniya Rostovskogo soveta narodnogo khozyaystva. (Hard facing) (Plows)

\$/277/63/000/001/002/017 A052/A126

AUTHOR:

Tkachev, V. N.

TITLE:

On the mechanism of corrosion fatigue of metals

PERIODICAL: Referativnyy zhurnal, otdel'nyy vypusk, 48. Mashinostroitel'nyye materialy, konstruktsii i raschet detaley mashin, no. 1, 1963, 4, abstract 1.48.19 ("Sb. rabot N.-i. in-ta tekhnol. mashinostr. Sovnarkhoz Rostovsk. ekon. adm. r-na", no. 1, 1960, 47 - 54)

Two theories dealing with the mechanism of corrosion fatigue are TEXT: compared and the process of crack formation in the elements of low-pressure boilers from the water side is studied. The character of corrosion-fatigue damages on the metal of locomotive-type boilers shows that under conditions in question the corrosion factor plays the primary part in the origination of corrosion-fatigue damages.

[Abstracter's note: Complete translation]

Card 1/1

CIA-RDP86-00513R001755920016-5" APPROVED FOR RELEASE: 07/16/2001

S/277/63/000/001/011/017 A052/A126

AUTHOR:

Tkachev, V. N.

TITLE:

On some properties of alloys

PERIODICAL: Referativnyy zhurnal, otdel'nyy vypusk, 48. Mashinostroitel'nyye materialy, konstruktsii i raschet detaley mashin, no. 1, 1963, 19, abstract 1.48.149 ("Sb. rabot N.-i. in-ta tekhnol. mashinostr. Sovnarkhoz Rostovsk. ekon. adm. r-na", no. 1, 1960, 78 - 82)

Mechanical properties ( $\sigma_{\!\!\! S}$  and  $\sigma_{\!\!\! b}$  at compression, the run-in capacity) were investigated and wear and corrosion-resistance tests were carried out of Zn-Al-alloy (up to 15% Al) also with Mg, Mn and Si additions, which were introduced in the form of master alloys. The tests have shown that 0.05% Mg raise corrosion-resistance of the alloy, an addition of more than 0.1% Mg reduces sharply the ductility and makes run-in of the alloy to the shaft neck worse. An addition of 0.4% Si reduces the ductility and causes shaft neck scoring at  $p = 20 \text{ kg/mm}^2$ . Among the alloys in question, UAMM 10-0,5 (TsAMts 10-0.5) has optimum properties and can be used as a bearing material. [Abstracter's note: Complete translation]

Card 1/1

\$/277/63/000/001/002/017 A052/A126

AUTHOR:

Tkachev, V. N.

TITLE:

On the mechanism of corrosion fatigue of metals

PERIODICAL: Referativnyy zhurnal, otdel'nyy vypusk, 48. Mashinostroitel'nyye materialy, konstruktsii i raschet detaley mashin, no. 1, 1963, 4, abstract 1.48.19 ("Sb. rabot N.-i. in-ta tekhnol. mashinostr. Sovnarkhoz Rostovsk. ekon. adm. r-na", no. 1, 1960, 47 - 54)

Two theories dealing with the mechanism of corrosion fatigue are TEXT: compared and the process of crack formation in the elements of low-pressure boilers from the water side is studied. The character of corrosion-fatigue damages on the metal of locomotive-type boilers shows that under conditions in question the corrosion factor plays the primary part in the origination of corrosion-fatigue damages.

[Abstracter's note: Complete translation]

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CIA-RDP86-00513R001755920016-5" **APPROVED FOR RELEASE: 07/16/2001** 

TKACHEV, V.N., kand.tekhn.nauk

New method for strengthening cutting parts of soil-cultivating machines. Mashinostroenie no.4:96-99 Jl-Ag '62. (MIRA 15:9)

1. Nauchno-issledovatel'skiy institut tekhnologii mashinostroyeniya,
Rostov-na-Donu.
(Cultivators)

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I KABHEY, U.K.

AUTHOR:

Tkachev, V.P., Engineer

98-7-13/20

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TITLE:

Improved Arrangement in Switching to Water or Cement in the Mixing Section of Concrete Plants (Uluchsheniye skhemy pereklyucheniya vody i sostavlyayushchikh betona v smesitel'nom

otdelenii betonnogo zavoda)

PERIODICAL:

Gidrotekhnicheskoye Stroitel'stvo, 1957, No 7, p 44, (USSR)

ABSTRACT:

Very often with concrete mixing plants with a frontal arrangement of the mixing machines (two per section), only one mixing machine was able to operate. This deficiency was due mainly to the fact, that the water faucet was hand-operated. The builders of the "Irtyshgesstroy" joined the supply of cement with that of water, installing a two-cylinder device, driven by compressed air, which operated the 2 valves of the water pipe and the 2-way chute of the cement hopper simultaneously, or alternately, thus giving both mixing

machines efficient and foolproof service.

This article contains 1 figure.

AVAILABLE:

Library of Congress

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VOLYNSKIY, Z.M., prof.; TKACHEV, V.P., kand.med.nauk

Use of radioactive iddine in coronary circulation disorders; clinical and experimental investigations. Terp.arkh. 31 no.9:12-20 S '59.

(MIRA 12:11)

1. Iz kafedry gospital 'noy terapii No.2 Voyenno-meditsinskoy ordena Lenina akademii imeni S.M. Kirova (nach. - prof. Z.M. Volynskiy).

(CORONARY DISZASE ther.)

(IODINE radioactive)

MARTIROSOV, K.S.; TKACHEV, V.P.

Examination of the functional state of the liver with the aid of radioactive Rose Bengal. Med.rad. 8 no.2:3-5 F'63 (MIRA 16:11)

1. Iz kafedry voyenno-morskoy i gospital noy terapii (nachal nik - prof. Z.M. Volynskiy) Voyenno-meditsinskoy ordena Lenina akademii imeni S.M. Kirova.

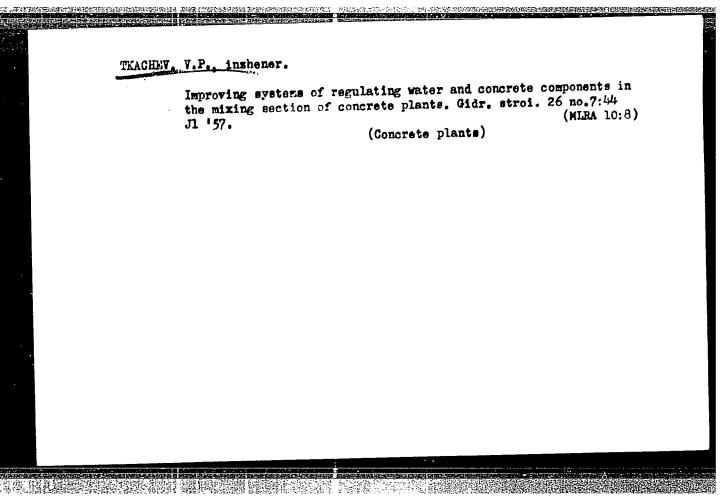
\*

SAGUNOV, V.G., kand. geologo-mineralogicheskikh nauk; TKACHEV, V.R.

Studying the waste products of mining and metallurgical enterprises of Kazakhatan as compound trace element fertilizers.

Vest. AN Kazakh. SSR 19 no.12:23-29 D '63. (MIRA 17.12)

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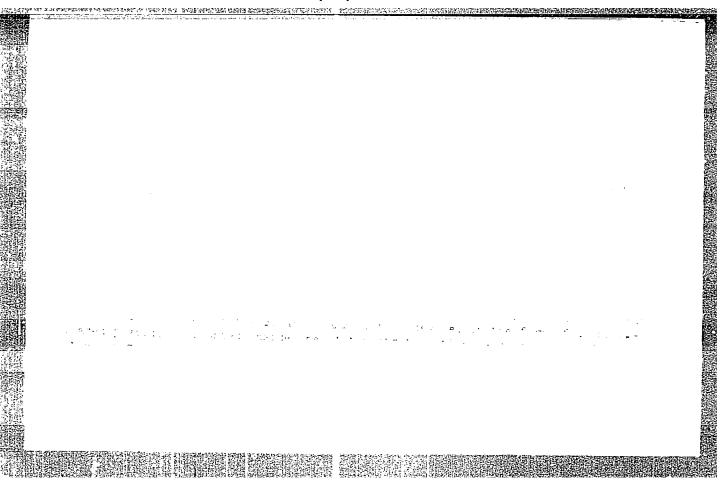


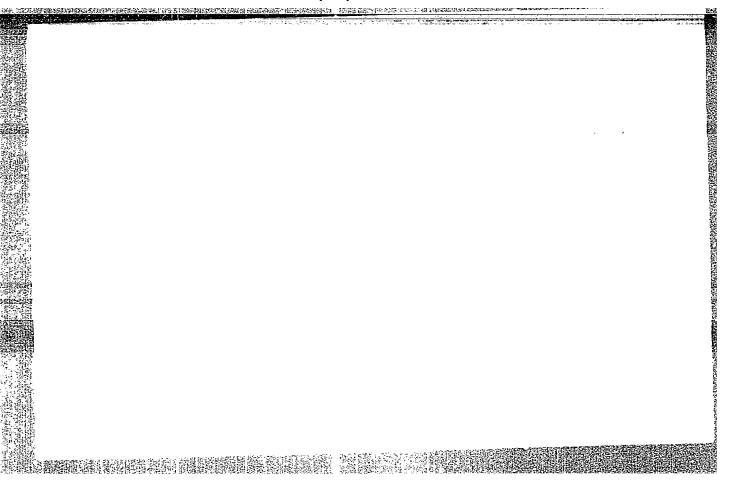
SAGUNOV, V.G. TRACHEV, V.R.

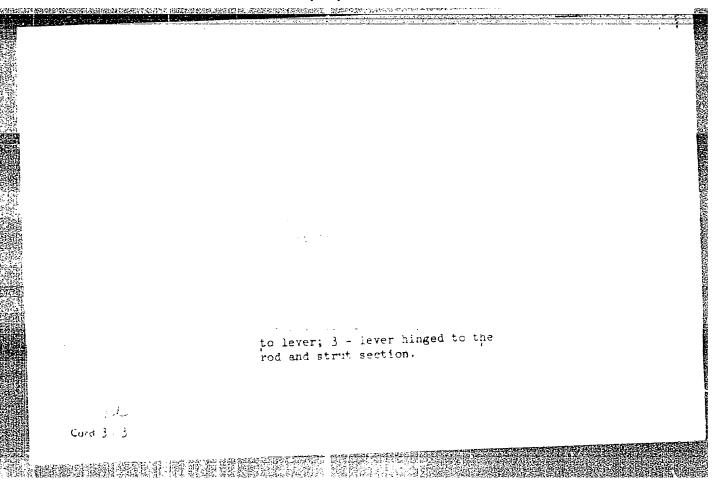
Phosphorite-bearing coal deposits in central and northern Kazakhstan. Izv. AN Kazakh. SSR. Ser. geol. no.1:55-63 '60. (MIRA 13:8)

(Kazakhstan--Phosphorites)

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With Descriptions of the Section of

TKACHEV, V.V.; LEYCHENKO, I.Ya.; OGANESOV, V.N.; ONISHCHENKO, I.S.;
NELIDOV, V.A.; SERKACHEV, O.V.; BOGIN, A.M.

Using separator mills in making cements of various specific surface areas. TSement 26 no.2:13-20 Mr-Ap '60.

(MIRA 13:6)

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BARON, L.I., doktor tekhn.nauk; TKACHEV, V.V., gornyy inzhener

Field testing of the simplified dry dust collector. Gig. 1 gm. 22 no.11:86-88 N '57.

1. Iz Komissii pir Akademii nauk SSSR po bor'be s silikozom 1 Nauchno-iseledovatel'akogo instituta "Vniiasbesttsement" (SILICOSIS, prev. & control in mining, prev. with dry dust collector (Rus))

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TKACHEV. V.V., mladshiy nauchnyy sotrudnik

Effect of the depth of tillage on physical properties of soil and crop yields. Isv.TSKhA no.3:109-126 '59. (MIRA 12:10)

(Tillage)

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TKACHEV, V.V., inzh.; SHIMECHEK, Ya. [Simecek, J.]

Evaluation of methods for dust control during the boring of upraises in soft rock. Bor'ba s sil. 6:180-183 '64 (MIRA 18:2)

1. Institut gigiyeny truda 1 professional'nykh zabolevanly AMM SSSR i Institut gigiyeny truda i professional'nykh zabolevaniy, Praga, Chekhoslovakiya.

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